

# Influence of Alkalis and Sulphates on the Mineralogical Composition of Clinker

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## 1 Introduction

The presence of minor constituents such as MgO, K<sub>2</sub>O, Na<sub>2</sub>O or SO<sub>3</sub> in the raw materials or in the fuels affects the clinkering process both thermodynamically, by modifying the phase stability volumes in the quaternary system CaO-SiO<sub>2</sub>-Al<sub>2</sub>O<sub>3</sub>-Fe<sub>2</sub>O<sub>3</sub> [1], and kinetically, by modifying the chemical and physical properties of the interstitial melt that exert a great influence on the crystal growth [2].

A recent study on the influence of SO<sub>3</sub> on the phase relationship in the quaternary system has shown that an increase in the SO<sub>3</sub> content causes a reduction of the primary phase volume of C<sub>3</sub>S and a change in the peritectic reaction occurring at the invariant point involving C<sub>3</sub>S, C<sub>2</sub>S, C<sub>3</sub>A, C<sub>4</sub>AF and liquid [3].

In a previous study [4] conducted on a rather large number of industrial clinkers, the quantitative phase analysis by means of X-Ray Diffraction and Rietveld Method (hereafter RQPA) had confirmed a strong influence of SO<sub>3</sub> and alkali contents on the mineralogical composition of clinker and consequently on the physical-mechanical properties of the resulting cements.

The present work reports about a further investigation into the influence of SO<sub>3</sub> and Na<sub>2</sub>O on the equilibrium phase composition of sintered mixes of pure components having the typical chemical modules of an industrial clinker.

## 2 Sample preparation

Six basic mixes of pure CaCO<sub>3</sub>, SiO<sub>2</sub>, Al<sub>2</sub>O<sub>3</sub> and Fe<sub>2</sub>O<sub>3</sub>, were prepared in order to obtain bulk compositions having lime saturation factor (LSF) from 0.92 to 0.98, alumina ratio (AR) from 1.15 to 2.00 and silica ratio (SR) equal to 2.50.

The range of AR values was chosen according to the quaternary phase diagram and so that they correspond to those points having an initial liquid composition above, at and below the invariant point [5].

SO<sub>3</sub>-bearing samples were prepared by using pure CaSO<sub>4</sub>·2H<sub>2</sub>O as supplementary raw material in order to have 0.75, 1.50 and 2.50 wt% of SO<sub>3</sub> in the sintered material.

For Na<sub>2</sub>O-bearing samples, pure Na<sub>2</sub>CO<sub>3</sub> was added to the six basic mixes, in order to have 0.75, 1.00 and 1.50 wt% of Na<sub>2</sub>O respectively in the sintered material.

The chemical compositions of all raw mixes were checked by means of X-ray fluorescence analyses.

Particular care was devoted to preparing the samples to guarantee not only the foreseen chemical compositions, but also good homogeneity.

For this reason, all the raw materials were ground to fineness lower than 40 μm and mixing was performed in cyclohexane.

The dried powders were also pre-calcined at 950°C in order to obtain CO<sub>2</sub>-free samples.

### 3 Experimental

Raw mixes were pressed into pellets to increase the contact surface between the different components.

After crushing, pellets were placed in small platinum tubes with an inner diameter of 5 mm.

For SO<sub>3</sub> and Na<sub>2</sub>O-bearing samples, platinum tubes were cap-sealed by using an arc-sealer, to suppress SO<sub>3</sub> and Na<sub>2</sub>O evaporation.

Burning was performed in a Deltech DT-31-VT vertical muffle by applying the following time-temperature profile: heating from 900 to 1500 °C at a rate of 6 °C/min, constant temperature of 1500°C for 90 min, cooling to 1300 °C at a rate of 4 °C/min, quenching to room temperature.

The phase diagram indicates that a certain amount of liquid phase coexists at equilibrium with C<sub>3</sub>S and C<sub>2</sub>S at 1500°C. The cooling rate applied from 1500 °C down to 1300°C was considered slow enough to achieve the chemical equilibrium during solidification.

All experiments were conducted in air; in this relatively oxidizing atmosphere, iron can be almost entirely considered as Fe<sup>3+</sup> and virtually no loss of iron occurs by its reaction with the platinum tube.

X-Ray Powder Diffraction (XRD) and microscopy analyses were performed on the sintered materials to determine type, amount and chemical composition of the phases produced in the sintering process.

XRD patterns have been collected using a SIEMENS D-5000 diffractometer with instrumental Bragg-Brentano geometry, equipped with a Cu-tube ( $\lambda = 1.5456 \text{ \AA}$ ) and a graphite monochromator on the diffracted beam.

The adopted experimental conditions were: tube power of 40KV, 40mA, fixed divergence and anti-scattering slits equal to 1°, receiving slit aperture of 0.1 mm, sample holder spinning of 30 rpm.

Diffraction patterns were collected from 10 to 70° 2 $\theta$ , at a scanning step of 0.02° 2 $\theta$  and counting time of 4 sec/step.

All the patterns were refined by means of the Rietveld method to obtain also quantitative information; these analyses were conducted using the TOPAS software [6].

Microstructure of the sintered materials was observed on polished sections under a Reflected Light Microscope (Reichert MeF3A) and a Scanning Electron Microscope (LEO 1450VP).

Moreover, the chemical composition of the mineralogical phases was determined by using an Energy Dispersive Spectrometer connected to the SEM (Gresham Sirius 10 detector and iXRF Iridium interface).

## 4 Results and discussion

Mineralogical compositions of the six basic clinkers obtained by RQPA and Bogue calculation are given in Table 1.

*Table 1: RQPA and Bogue mineralogical composition of the six basic clinkers.*

sample	C <sub>3</sub> S (wt%)		C <sub>2</sub> S (wt%)		C <sub>3</sub> A (wt%)		C <sub>4</sub> AF (wt%)	
	RQPA	Bogue	RQPA	Bogue	RQPA	Bogue	RQPA	Bogue
LSF 0.92, AR 1.15	69.6	59.7	14.5	21.4	6.4	5.9	9.5	13.1
LSF 0.92, AR 1.38	59.5	58.2	24.4	22.4	7.6	7.6	8.5	11.8
LSF 0.92, AR 2.00	57.3	55.3	25.1	24.3	12.7	11.1	5.0	9.3
LSF 0.98, AR 1.15	80.7	74.4	4.4	7.5	5.6	5.6	9.3	12.5
LSF 0.98, AR 1.38	75.3	72.9	6.3	8.4	8.2	7.3	10.3	11.3
LSF 0.98, AR 2.00	74.8	70.2	6.6	10.2	13.2	10.6	5.3	8.9

The content of the main constituents in the samples reflects the different chemical compositions of the starting mixes: the C<sub>3</sub>S content increases with increasing LSF and decreasing AR, while C<sub>3</sub>A content increases with increasing AR; trends of C<sub>2</sub>S and C<sub>4</sub>AF contents are opposite to those of C<sub>3</sub>S and C<sub>3</sub>A respectively.

Some deviations of RQPA composition compared to the theoretical Bogue values are most apparent.

The C<sub>3</sub>S content is higher and the total content in aluminate phases (C<sub>3</sub>A+C<sub>4</sub>AF) is usually lower except for sample with LSF=0.98 and AR=1.38.

SEM-EDS analyses show that these differences are probably due to the inclusion of foreign elements in the lattice of clinker phases rather than non-equilibrium conditions during the experiments.

In fact, the lower total aluminate content is clearly due to the inclusion of Al and Fe in the silicate phases (see Fig. 1 and 2) that reduces their availability for aluminate and ferrite formation.

As a consequence, some of the lime not combined in the aluminate phases contributes to the formation of additional C<sub>3</sub>S.

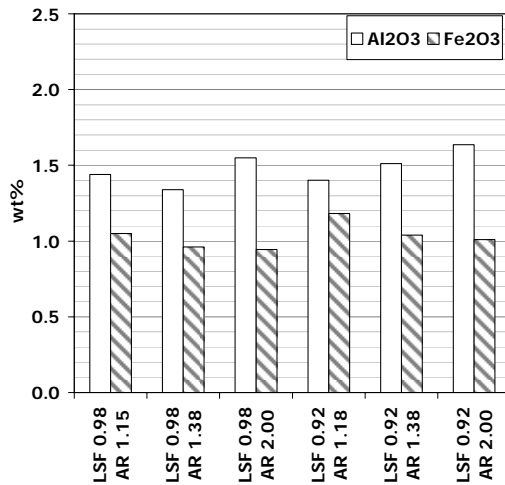


Fig. 1: Chemical composition of C<sub>3</sub>S obtained by SEM-EDS analysis.

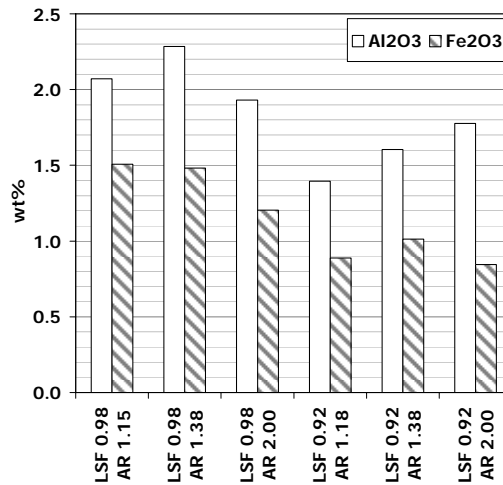


Fig. 2: Chemical composition of C<sub>2</sub>S obtained by SEM-EDS analysis.

The microstructural characteristics of the sintered materials confirm the good homogeneity of the raw mixes, an adequate burning time and an appropriate cooling rate to achieve equilibrium conditions.

In all samples alite appears as idiomorphous crystals with dimensions of about 20 μm, while belite is homogeneously distributed showing rounded shape crystals with average dimensions of about 35 μm.

Smaller crystal sizes are observed in the samples with the highest LSF or the highest AR.

Interstitial phase appears coarsely crystallized and made only by cubic C<sub>3</sub>A and C<sub>4</sub>AF.

The sample porosity is generally low for all the clinkers.

These microstructural characteristics do not differ much from those of industrial clinkers.

#### 4.1 Influence of SO<sub>3</sub>

Eighteen SO<sub>3</sub>-bearing raw mixes were sintered to evaluate the influence of SO<sub>3</sub> on the mineralogical composition of clinker.

Results of the RQPA are given in Table 2.

A small amount of residual CaSO<sub>4</sub> (anhydrite) was detected in the sintered materials containing 2.5 wt% of SO<sub>3</sub>.

A change in the amount of C<sub>3</sub>S and C<sub>2</sub>S as a function of the SO<sub>3</sub> content is apparent.

The C<sub>3</sub>S/C<sub>2</sub>S wt. ratio is strongly reduced in SO<sub>3</sub>-bearing samples respect to their correspondent SO<sub>3</sub>-free samples (see Fig. 3).

In the samples containing 2.5 wt% of SO<sub>3</sub>, C<sub>3</sub>S is practically undetectable and a large amount of free lime is found.

These results are in good agreement with previous studies showing that the primary phase volume of  $C_3S$  tends to shrink with the increase of the  $SO_3$  content and finally disappears [3].

Table 2: RQPA results for the clinkers containing different amounts of  $SO_3$ . Results are expressed as wt%.

sample	$SO_3$	$C_3S$	$C_2S$	$C_3A$	$C_4AF$	Free lime	$CaSO_4$
	0.0	69.6	14.5	6.4	9.5	-	-
LSF 0.92	0.75	53.1	31.4	5.5	10.0	-	-
AR 1.15	1.5	40.1	47.7	3.9	8.3	-	-
	2.5	4.4	72.5	4.1	11.2	7.7	0.2
	0.0	59.5	24.4	7.6	8.5	-	-
LSF 0.92	0.75	55.4	26.5	9.5	8.6	-	-
AR 1.38	1.5	51.4	33.9	5.5	9.1	-	-
	2.5	2.1	70.7	4.6	9.6	6.7	0.3
	0.0	57.3	25.1	12.7	5.0	-	-
LSF 0.92	0.75	49.0	34.9	11.3	4.8	-	-
AR 2.00	1.5	46.1	38.9	11.2	3.8	-	-
	2.5	0.0	72.2	11.8	8.3	6.6	0.6
	0.0	80.7	4.4	5.6	9.3	-	-
LSF 0.98	0.75	59.6	22.7	7.0	10.8	-	-
AR 1.15	1.5	60.1	23.9	5.9	10.1	-	-
	2.5	0.0	72.4	3.0	13.3	10.9	0.3
	0.0	75.3	6.3	8.2	10.3	-	-
LSF 0.98	0.75	60.8	22.4	8.3	8.5	-	-
AR 1.38	1.5	64.0	21.1	6.9	8.0	-	-
	2.5	0.0	71.5	4.5	13.5	10.3	0.2
	0.0	74.8	6.6	13.2	5.3	-	-
LSF 0.98	0.75	50.2	30.7	14.0	5.0	-	-
AR 2.00	1.5	60.9	22.4	9.4	7.4	-	-
	2.5	0.0	69.3	7.7	12.4	10.4	0.2

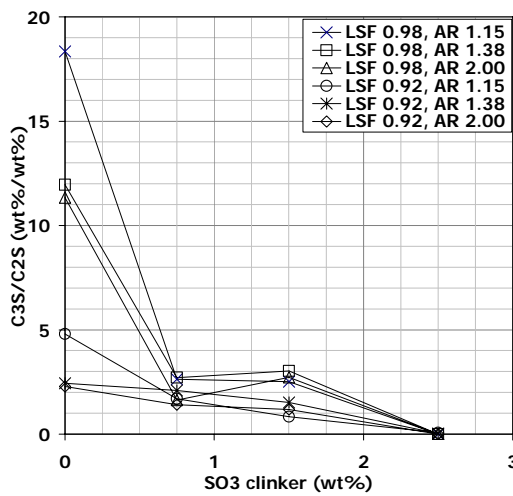


Fig. 3:  $C_3S/C_2S$  wt. ratio as a function of  $SO_3$  content in the clinkers

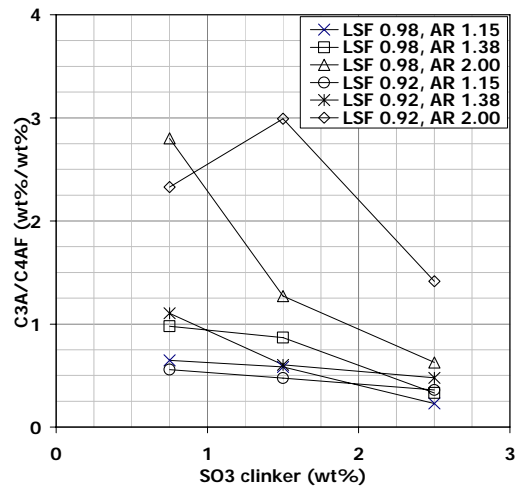


Fig. 4:  $C_3A/C_4AF$  wt. ratio as a function of  $SO_3$  content in the clinkers

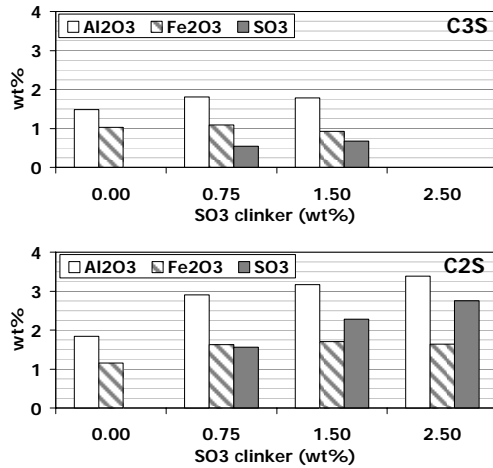


Fig. 5: Al<sub>2</sub>O<sub>3</sub>, Fe<sub>2</sub>O<sub>3</sub> and SO<sub>3</sub> contents in C<sub>3</sub>S and C<sub>2</sub>S as obtained by SEM-EDS analysis of the clinkers containing different amounts of SO<sub>3</sub>

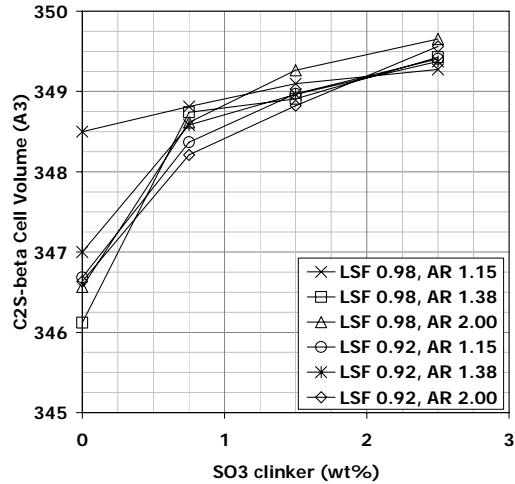


Fig. 6: β-C<sub>2</sub>S cell volume variation as a function of SO<sub>3</sub> content in the clinkers

The C<sub>3</sub>A content decreases with increasing SO<sub>3</sub> contents in all samples. The C<sub>4</sub>AF content remains constant or slightly increases for SO<sub>3</sub> content up to 1.5 wt%.

In the samples with 2.5 wt% of SO<sub>3</sub>, the C<sub>4</sub>AF content considerably increases, since a peritectic reaction  $L + C_2S \rightarrow CaO + C_4AF$  occurs [3].

As a consequence the C<sub>3</sub>A/C<sub>4</sub>AF wt. ratio is shifted to smaller values, with one exception (Fig. 4).

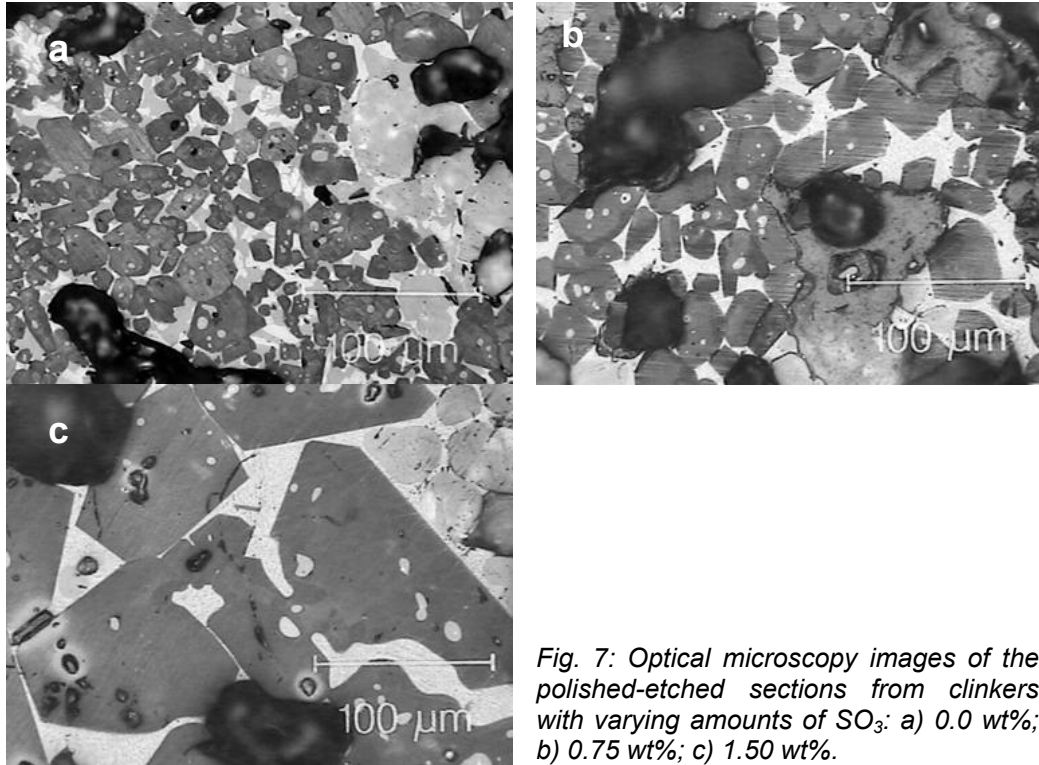
The chemical composition obtained by SEM-EDS shows that sulphur is exclusively incorporated in the silicate phases and preferentially in C<sub>2</sub>S, confirming other previous observations [7].

Both Al and Fe are incorporated in larger amounts in C<sub>2</sub>S than in C<sub>3</sub>S (see Fig. 5).

The Al and Fe content in silicate phases rises by the increase of SO<sub>3</sub> and this effect is especially apparent for Al.

The higher amount of inclusions in the silicates structure is also supported by the increase in the C<sub>2</sub>S cell volume, as detected by XRD for the sample containing SO<sub>3</sub> (see Fig. 6).

According XRD patterns [8], C<sub>3</sub>S seems to be exclusively present as M1 polymorph and its crystal size is also increased by the presence of SO<sub>3</sub> for the well-known mineralizing effect due to sulfate (see Fig. 7) [9, 10].



*Fig. 7: Optical microscopy images of the polished-etched sections from clinkers with varying amounts of SO<sub>3</sub>: a) 0.0 wt%; b) 0.75 wt%; c) 1.50 wt%.*

## 4.2 Influence of Na<sub>2</sub>O

Eighteen Na<sub>2</sub>O-bearing raw mixes were sintered to evaluate the influence of Na<sub>2</sub>O on the mineralogical composition of clinker.

Results of the RQPA are given in Table 3.

The addition of Na<sub>2</sub>O to the mixes leads to a strong modification of the mineralogical composition of the clinkers as detected by XRD and optical microscopy (see Fig. 8 and 9).

In fact, in presence of Na<sub>2</sub>O, orthorhombic C<sub>3</sub>A appears and for Na<sub>2</sub>O contents higher than 1.0 wt% it is the only polymorph present.

The total C<sub>3</sub>A content increases by 4 wt% in clinkers containing Na<sub>2</sub>O, while the C<sub>4</sub>AF content decreases by 2 wt%.

Na<sub>2</sub>O in the samples causes also the stabilization of high temperature polymorphs of C<sub>2</sub>S.

In samples with 0.75 and 1.0 wt% of Na<sub>2</sub>O beside the β form also the α' and α forms are present and their content tends to increase with increasing Na<sub>2</sub>O.

Optical microscopy observations highlight a modification of the lamellar structure of belite crystals.

At increasing Na<sub>2</sub>O contents, the frequency of striations is lower and they become coarser.

Striations in belite arise upon cooling through a α-to-α' transition and they split in two when the transition from α'<sub>L</sub> to β occurs.

These microstructural characteristics confirm that the increase of Na<sub>2</sub>O content causes the stabilization of high temperature polymorphs of belite. SEM-EDS analyses show that the larger portion of Na is incorporated in the aluminate phases, mainly in C<sub>3</sub>A, and only to a lesser extent in the silicate phases, with higher values found in C<sub>2</sub>S than in C<sub>3</sub>S.

Its replacement for Ca increases in all phases as the Na<sub>2</sub>O content of the clinkers increases, reaching a maximum value of about 4 wt% in C<sub>3</sub>A.

This substitution leaves additional lime available for the supplementary formation of C<sub>3</sub>A and C<sub>3</sub>S, as shown by XRD analyses.

The SEM-EDS analysis reveals that in presence of Na<sub>2</sub>O, C<sub>3</sub>S has a lower CaO/SiO<sub>2</sub> wt. ratio and the aluminate phases have a SiO<sub>2</sub> content that is almost twice as great.

In samples with LSF=0.98, a certain amount of free lime is detected for high Na<sub>2</sub>O contents, while this does not occur in the same samples Na<sub>2</sub>O-free or in samples with LSF=0.92 (see Table 3).

Based on these observations, it can be supposed that the upper limit of the lime saturation factor to prevent primary crystallization of free lime is reduced.

This could be justified by the primary stability volume of C<sub>3</sub>S moving away from the CaO corner in the quaternary diagram.

*Table 3: RQPA results for the clinkers containing different amount of Na<sub>2</sub>O. Results are expressed as wt%.*

<i>sample</i>	<i>Na<sub>2</sub>O</i>	<i>C<sub>3</sub>S</i>	<i>β-C<sub>2</sub>S</i>	<i>α'-C<sub>2</sub>S</i>	<i>α-C<sub>2</sub>S</i>	<i>C<sub>2</sub>S<sub>TOT</sub></i>	<i>C<sub>3</sub>A<sub>cube</sub></i>	<i>C<sub>3</sub>A<sub>ortho</sub></i>	<i>C<sub>3</sub>A<sub>TOT</sub></i>	<i>C<sub>4</sub>AF</i>	<i>Free lime</i>
	0.0	69.6	14.5	-	-	14.5	6.4	-	6.4	9.5	-
<i>LSF 0.92</i>	0.75	69.5	-	11.5	1.6	13.2	-	10.0	10.0	7.4	-
<i>AR 1.15</i>	1.0	69.6	-	9.2	3.6	12.8	-	10.8	10.8	6.8	-
	1.5	75.0	-	-	5.5	5.5	-	14.3	14.3	5.2	-
	0.0	59.5	24.4	-	-	24.4	7.6	-	7.6	8.5	-
<i>LSF 0.92</i>	0.75	60.4	5.4	14.1	3.4	22.9	4.7	5.8	10.5	6.2	-
<i>AR 1.38</i>	1.0	62.3	-	14.7	4.7	19.4	-	12.9	12.9	5.4	-
	1.5	70.5	-	2.5	7.6	10.0	-	14.9	14.9	4.5	-
	0.0	57.3	25.1	-	-	25.1	12.7	-	12.7	5.0	-
<i>LSF 0.92</i>	0.75	57.4	8.2	12.3	2.5	23.0	4.6	11.4	16.0	3.7	-
<i>AR 2.00</i>	1.0	62.1	-	14.1	3.3	17.4	-	17.0	17.0	3.5	-
	1.5	67.1	-	8.0	6.5	14.5	-	15.1	15.1	3.3	-
	0.0	80.7	4.4	-	-	4.4	5.6	-	5.6	9.3	-
<i>LSF 0.98</i>	0.75	77.6	0.4	4.5	0.0	5.0	-	12.3	12.3	5.2	-
<i>AR 1.15</i>	1.0	80.2	-	0.0	2.7	2.7	-	11.9	11.9	5.2	-
	1.5	80.5	-	0.0	0.9	0.9	-	13.2	13.2	5.3	-
	0.0	75.3	6.3	-	-	6.3	8.2	-	8.2	10.3	-
<i>LSF 0.98</i>	0.75	78.4	-	1.8	1.7	3.5	-	12.6	12.6	5.6	-
<i>AR 1.38</i>	1.0	79.9	-	0.2	2.3	2.5	-	11.6	11.6	5.4	0.6
	1.5	78.7	-	0.0	0.9	0.9	-	16.0	16.0	3.2	1.3
	0.0	74.8	6.6	-	-	6.6	13.2	-	13.2	5.3	-
<i>LSF 0.98</i>	0.75	74.9	1.5	3.4	1.8	6.7	-	14.4	14.4	4.0	-
<i>AR 2.00</i>	1.0	75.7	-	2.6	1.8	4.6	-	16.4	16.4	3.2	-
	1.5	79.4	-	1.5	1.9	3.4	-	13.7	13.7	2.8	0.6



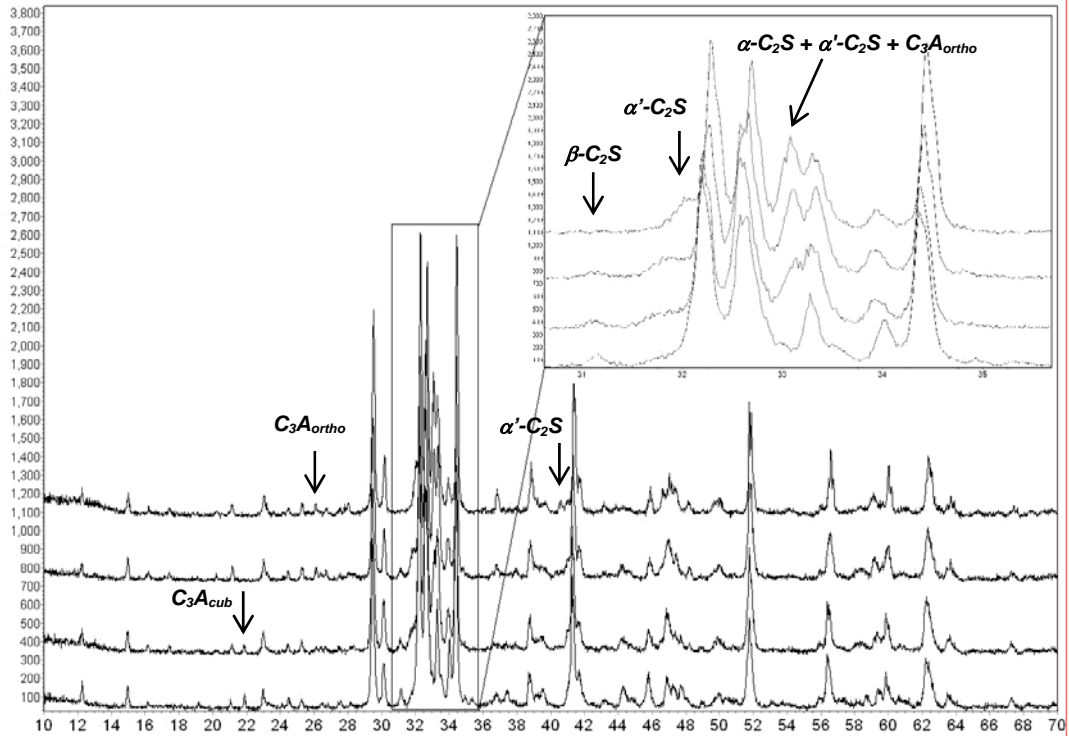


Fig. 8: X-ray patterns of the clinkers with different  $\text{Na}_2\text{O}$  contents.  $\text{C}_3\text{A}_{\text{cub}}$  peak at  $21.9^\circ 2\theta$  disappears for  $\text{Na}_2\text{O}$  contents  $>0.5$  wt% while  $\text{C}_3\text{A}_{\text{ortho}}$  peak at  $26.1^\circ 2\theta$  becomes detectable. The intensity of  $\beta\text{-C}_2\text{S}$  peaks at  $31.2$  and  $37.5^\circ 2\theta$  decreases with increasing  $\text{Na}_2\text{O}$  contents and the peaks of  $\alpha'\text{-C}_2\text{S}$  at  $40.5^\circ 2\theta$  and  $\alpha\text{-C}_2\text{S}$  at  $32^\circ 2\theta$  appear.

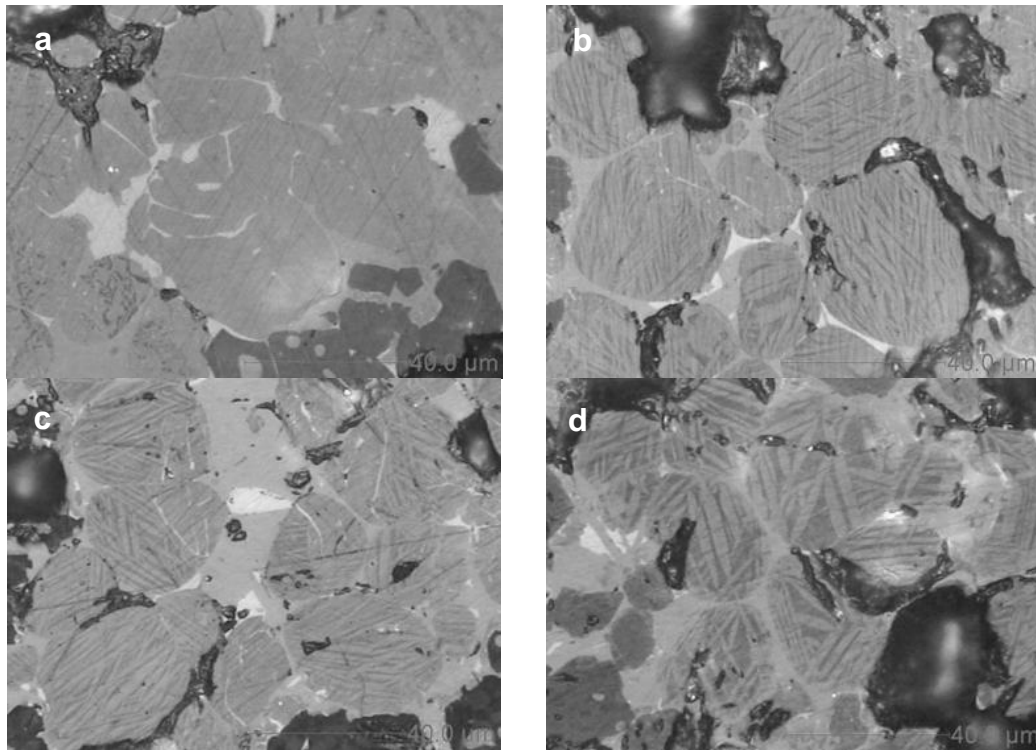


Fig. 9: Optical microscopy images of the polished-etched sections from clinkers with varying amounts of  $\text{Na}_2\text{O}$ : a) 0.0 wt%; b) 0.75 wt%; c) 1.0 wt%; d) 1.5 wt%.

SEM-EDS analyses show that the iron content in  $C_3A$  increases from 5-6 wt% in the clinker having the lowest  $Na_2O$  content to 9-15 wt% in the clinkers with the highest  $Na_2O$  contents.

Moreover, the increase of  $C_3A/C_4AF$  wt. ratio (Table 3) suggests that the presence of  $Na_2O$  causes a decrease of the  $Al_2O_3/Fe_2O_3$  ratio of the invariant point.

XRD pattern inspection shows that  $C_3S$  is exclusively in the M3 form [7] and its crystal size is also increased by the presence of  $Na_2O$ .

## 5 Conclusions

As the  $SO_3$  content in the sintered materials increases, the  $C_3S$  primary phase volume is reduced in the quaternary phase diagram, resulting in a decrease of  $C_3S/C_2S$  wt. ratio.

For the samples considered, 2.5 wt. % is the limit of  $SO_3$  content at which  $C_3S$  is not formed.

Sulphur is preferentially incorporated in the silicate phases (mainly  $C_2S$ ) and the inclusions of Al and Fe increase as  $SO_3$  increases.

For this reason, the aluminates content decreases with increasing  $SO_3$  content, such as the  $C_3A/C_4AF$  ratio.

The  $C_4AF$  content considerably increases only in those samples with 2.5 wt% content of  $SO_3$ , due to the occurrence at the invariant point of the peritectic reaction  $L+C_2S \rightarrow CaO+C_4AF$ .

The addition of  $Na_2O$  to the mixes strongly modifies the mineralogical composition of the sintered materials: orthorhombic  $C_3A$  appears and becomes the only  $C_3A$  polymorph present when the  $Na_2O$  content is higher than 1.0 wt%.

Na is mainly incorporated in  $C_3A$  and its content limit is 4 wt% (expressed as  $Na_2O$ ). Na is partly incorporated in  $C_2S$ , causing the stabilization at room temperature of the forms  $\alpha$  and  $\alpha'$ .

The increase of the  $Na_2O$  content in the clinkers leads to a  $C_2S$  content decrease and a  $C_3S$  content increase.

For high amounts of  $Na_2O$ , the appearance of the equilibrium free lime in the clinkers with an LSF of 0.98 is observed.

This can be explained by a reduction of the maximum acceptable CaO content of the mixes with  $Na_2O$  that derives from the fact that the  $C_3S$  primary stability volume moves away from the CaO corner in the quaternary system.

At the same time, the decrease in the  $Al_2O_3$  to  $Fe_2O_3$  ratio of the invariant point causes an increase of the  $C_3A/C_4AF$  wt. ratio.

These results justify previous observations concerning the effects of  $SO_3$  and  $Na_2O$  on the mineralogical composition of industrial clinker [4].

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